

**Amendments to the Specification:**

Please replace the paragraph beginning at page 19, line 12, with the following rewritten paragraph:

-- The three gyro 76d-76f input axes and three accelerometer 74d-74f input axes are preferably mutually orthogonal at the two 180° degree apart inner gimbal stops, and in between if the inner gimbals rotate in parallel, which can be accomplished by using one inner gimbal motor 40b that drives a gear chain which rotates ~~gyrocompasses~~ gyros 76d-76f and accelerometers 74d-74f stacked in an alternating configuration as shown in Fig. 8. --

Please replace the paragraph beginning at page 25, line 24, with the following rewritten paragraph:

-- (6) The outer gimbal is indexed or rotated  $-180^\circ$  with data being collected during the rotation. It is important for calibration reasons that the outer gimbal be rotated  $-180^\circ$  rather than  $+180^\circ$ , even though the outer gimbal has complete rotary freedom. The effects of ~~gyrocompass~~ gyro bias and the Earth's rotation rate increases the magnitude of the integral of the ~~gyrocompass~~ gyro output in a  $180^\circ$  rotation for one direction of rotation, and decreases this magnitude for the other direction of rotation. Thus even if not included exactly correctly in analyzing the data, the ~~gyrocompass~~ gyro scale factor calibration using the combined  $+180^\circ$  and  $-180^\circ$  slews is insensitive to these effects; --



Please replace the paragraph beginning at page 27, line 15, with the following rewritten paragraph:

-- If the gyrocompass information is used to determine azimuth, the assumption is preferably made that drill pipe 18 is stationary during the gyrocompass operation. Since the drill pipe is lifted off the bottom of the hole when a length of pipe is added, there could be some rotation of the drill pipe. The magnetometer data could be biased in its measurement of the Earth's magnetic field direction, but the change in magnetometer direction determination between the start and end of data taking at each gyrocompass position and across all four gyrocompass positions can be used to correct the ~~gyrocompass gyro~~ data and the accelerometer data for the rotation of the drill string during the gyrocompass operation, if there were a three-axis magnetometer in the system. --

Please replace the paragraph beginning at page 28, line 19, with the following rewritten paragraph:

-- Assume that the ~~gyrocompass gyro~~ and accelerometer input axes (IA) in the inner gimbal frame have the orientations

$$IA_1 = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, \quad IA_2 = \begin{bmatrix} 0 \\ \cos 45^\circ \\ \sin 45^\circ \end{bmatrix}, \quad IA_3 = \begin{bmatrix} 0 \\ -\sin 45^\circ \\ \cos 45^\circ \end{bmatrix} \quad (2)$$

with  $IA_1$  parallel to the outer gimbal axis at the cardinal gyrocompass positions and  $IA_2$  and  $IA_3$  at  $45^\circ$  angles to the inner gimbal axis. --



Please replace the paragraph beginning at page 29, line 3, with the following rewritten paragraph:

-- Let ( $\omega_1, \omega_2, \omega_3$ ) in the outer gimbal frame be the input to a sensor (Earth's rotation inertial angular velocity for a ~~gyrocompass~~ gyro, specific force or nongravitational acceleration reaction up to gravity pulling down for an accelerometer). --

Please replace the paragraph beginning at page 33, line 20, with the following rewritten paragraph:

-- Since the  $180^\circ$  slew between positions takes much less time than the gyrocompass dwells at the positions, the scale factor calibration can be less accurate than the gyrocompass calibration, offset however by having a larger rate input during the slew. Preferably, there are commensurate times for dwelling at a position and for slewing between positions. For instance, if the gyrocompass accuracy can measure the Earth's rotation vector direction to  $10^{-3}$  radians, then the gyrocompass slew calibration should measure ~~gyrocompass~~ gyro scale factor to at least a part-in-a-thousand accuracy, unless the ~~gyrocompass~~ gyro scale factor were adequately stable from the surface calibration. Better scale factor accuracy is desirable for navigating while drilling, but the requirements while drilling can be ameliorated by outer gimbal  $\pm 360^\circ$  carouseling relative to inertial space and by  $\pm 180^\circ$  inner gimbal indexing during drilling, and by external aids (such as from length of pipe going down the drill hole and from magnetometer data, as described below). --

Please delete the section heading at page 31, line 10.

Please add the following new section heading before the paragraph beginning at page 31, line 11.

-- Calibration of Gyro Scale Factors during Gyrocompass Slews --